# Hydrometeorological analyses relevant to Jabiluka 

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Hydrology Unit

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## 1 Introduction

In response to a request from the Supervising Scientist, the Bureau of Meteorology Hydrology Unit has undertaken a range of hydrometeorological analyses relevant to Jabiluka for input to projects being undertaken by the University of Melbourne and CSIRO. The analyses undertaken for this report included:

- Extraction of rainfall, evaporation and other relevant climate data from the Bureau's climatological database;
- Infilling of missing data to provide a complete, long term, record of daily rainfall;
- Analysis of the annual series (September to August) of rainfall data to determine the best estimate of the $1: 10,000 \mathrm{AEP}$ annual rainfall including the provision of confidence limits on the estimates;
- Comment on the methodology used in the Jabiluka EIS and associated documents and discussion of any other techniques which may be used to estimate the $1: 10,000$ AEP annual rainfall; and,
- Derivation of the design Probable Maximum Precipitation estimates of relevance to the Jabiluka project area.


## 2 Availability of rainfall, evaporation and other relevant climate data

The Bureau of Meteorology's climate database was analysed to determine the availability of rainfall, evaporation and other relevant climate data. Table 1 identifies the stations found when implementing the Hydrology Unit's rainfall station and climate search procedure.

Table 1 Rainfall, evaporation and climate data stations in the region surrounding the Jabiluka project

| Proximity | Rainfall | Record | Evaporation | Record | Climate | Record |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Within 100 km | Oenpelli Jabiru Airport Jabiru Council Kapalga CSIRO Mudginberri Munmalary | $\begin{aligned} & 1911-1998 \\ & 1972-1998 \\ & 1984-1998 \\ & 1988-1994 \\ & 1965-1980 \\ & 1965-1980 \end{aligned}$ | Jabiru Airport | 1974-1998 | Oenpelli Jabiru Airport | $\begin{aligned} & 1979-1998 \\ & 1979-1998 \end{aligned}$ |
| Within next 100 km | Cape Don Koolpinyah Middle Point Maningrida Wurruwi Pine Creek | $\begin{aligned} & 1919-1988 \\ & 1914-1972 \\ & 1959-1998 \\ & 1958-1998 \\ & 1917-1998 \\ & 1875-1998 \end{aligned}$ | Middle Point Maningrida | $\begin{aligned} & 1966-1998 \\ & 1968-1998 \end{aligned}$ | Cape Don Middle Point Maningrida Wurruwi | $\begin{gathered} 1961-1988 \\ 1966-1998 \\ 1968-1998 \\ 1961-1998 \end{gathered}$ |
| Key sites further away | Darwin Airport Darwin PO Katherine | $\begin{aligned} & 1942-1998 \\ & 1870-1961 \\ & 1874-1998 \end{aligned}$ | Darwin Airport | 1942-1998 | Darwin A/P <br> Darwin PO <br> Katherine | $\begin{aligned} & 1942-1998 \\ & 1900-1961 \\ & 1969-1998 \end{aligned}$ |

Table 2 lists the details of the data that were supplied by the Bureau's National Climate Centre to the University of Melbourne for analyses of the relationships between the data recorded at the various sites.

Table 2 Details of data provided to the University of Melbourne

| Data type | Station number | Station name |
| :--- | :---: | :---: |
| Daily and monthly precipitation | 014198 | Jabiru Airport |
| data | 104400 | Maningrida |
|  | 014090 | Middle Point |
|  | 014016 | Darwin PO |
|  | 014015 | Darwin Airport |
| Daily and monthly evaporation | 014042 | Oenpelli |
| data (Pan) | 014198 | Jabiru Airport |
|  | 014400 | Maningrida |
| Daily | 014090 | Middle Point |
| Maximum temperature | 014015 | Darwin Airport |
| Minimum temperature | 014198 |  |
| Wind run | 014198 | Jabiru Airport |
| Sunshine hours | 014198 | Jabiru Airport |
| Other climate data | 014198 | Jabiru Airport |
| 3-hour $T_{\text {dry }}$ | 014198 | Jabiru Airport |
| 3-hour T wet | 014198 |  |

## 3 Infilling of missing rainfall and evaporation data

Following discussions with the University of Melbourne after their analysis of the available climate data, the Bureau of Meteorology was requested to infill the daily rainfall record for the Oenpelli site and the monthly rainfall and evaporation data for the Jabiru Airport site.

The accumulated daily rainfall data for Oenpelli were infilled by distributing the accumulated totals by the pattern of rainfall at the nearest rainfall station for which records were available. The missing data were infilled using the data from the closest available station. If a monthly total was available for Oenpelli, the nearest station data were adjusted by multiplication by the ratio of the Oenpelli monthly total to the nearest station monthly total. If an Oenpelli monthly total was not available, the nearest station data were adjusted by multiplication by the ratio of the annual mean rainfall at Oenpelli to the annual mean rainfall at the nearest station.

In summary, there was very little missing data in the Oenpelli daily rainfall record and the 88 years of data (1911-1998) is an excellent record.

The monthly rainfall and evaporation data for Jabiru Airport was provided by the ERA (Energy Resources of Australia). A check of these data against the Jabiru Airport data in the Bureau of Meteorology's database indicated that these data sets were similar, but the ERA
data set was more complete and up to date. As only the monthly and annual data were to be used from this site, it was not necessary to infill the daily record.

The above data sets were supplied to Melbourne University for them to undertake the Hydrological Modelling Study of Water Management at the Jabiluka Site (Chiew \& Wang, 1999).

## 4 Estimation of 1:10,000 AER annual rainfall

The annual rainfall totals (September to August) were derived using the data sets described above. The $1: 10,000$ AEP annual rainfall was estimated for both the Oenpelli and Jabiru Airport rainfall stations using all of the available data. This estimate of the $1: 10,000$ AEP annual rainfall is based on the assumption of a statistically stationary climate and does not take account of any expected or unexpected impact of the enhanced greenhouse effect. Furthermore, there is no known method of reliably estimating the $1: 10,000$ AEP annual rainfall from a sample of the order of 100 years. The method employed relies on the assumption that annual rainfalls which reasonably fit a normal distribution for the sample of available data, continues to do so into the extreme high end of the actual distribution. Nevertheless, where, for practical reasons, an estimate must be made, this is the main method currently employed in Australia.

### 4.1 Analysis of Oenpelli annual rainfall data

The length of rainfall record for Oenpelli is 88 years (1911-1998) and the annual characteristics of the annual rainfall data are given in table 3 . These values were derived using the data provided in Appendix A. The maximum and minimum observed annual rainfall during the period are $2012 \mathrm{~mm}(1975-76)$ and $720 \mathrm{~mm}(1941-42)$ respectively.

Table 3 The annual characteristics of Oenpelli rainfall data

| Statistic | Magnitude | Standard Error |
| :--- | :---: | :---: |
| Mean $(\mathrm{mm})$ | 1397 | 30.3 |
| Standard deviation $(\mathrm{mm})$ | 284.5 | 21.4 |
| Coefficient of skewness | -0.018 | 0.257 |

Chi-squared test results (test statistic - 4.39/chi-square value ( $0.05 \%$ ) - 9.49) and Kolmogorov Smirnov test results (test statistic $-0.05881 /$ value -0.145 ) indicate that the annual rainfall data series for Oenpelli is normally distributed. It should also be noted that the coefficient of skewness of the annual rainfall series is small. The use of the normal distribution is also supported by the analyses undertaken by Vardavas (1992). The plot of the observed data and the fitted line are shown in figure 1 . The x -axis has a normal probability scale and plotting position is determined by the rank of annual rainfall (plotted on the y-axis). Data that are normally distributed plot as a straight line on this type of graph. The 1:10,000 AEP annual rainfall estimate is 2455 mm with a standard error of 85 mm . This estimate was derived using equation (1) (IE Aust 1987):

$$
\begin{equation*}
Q_{y}=M+K_{y} S \tag{1}
\end{equation*}
$$

where: $\mathrm{Q}_{\mathrm{y}}=$ the annual rainfall having an Annual Exceedance Probability (AEP) of 1 in y ,
$\mathrm{M}=$ mean of annual rainfall series,

$$
\begin{aligned}
& \text { S = standard deviation of the annual rainfall series, } \\
& K_{y}=\text { frequency factor for the normal distribution for AEP of } 1 \text { in } \mathrm{y} \text {, and } \\
& \text { y }=10000 \text { years (in this case). }
\end{aligned}
$$

In the case of the normal distribution equation (1) can be expressed as:

$$
\begin{equation*}
Q_{10,000}=M+Z_{0.9999} \times S \tag{2}
\end{equation*}
$$

where: Z is the z -statistic, which simply specifies the distance of a point from the mean in units of standard deviation. The subscript to Z denotes the 0.9999 quantile (the 99.99 percentile). From normal probability tables, $\mathrm{Z}_{0.9999}=3.719$.
The $95 \%$ confidence limit for this estimate, rounded to the nearest 10 mm is $\mathbf{2 4 6 0} \pm \mathbf{1 7 0} \mathbf{~ m m}$.


Figure 1 Distribution of annual rainfall for Oenpelli

### 4.2 Analysis of Jabiru Airport annual rainfall data

The length of the rainfall record for Jabiru Airport is 27 years (1972-1998) and the annual characteristics of the annual rainfall data are given in table 4 . These values were derived from the data presented in Appendix A. The maximum and minimum observed annual rainfall during the period are 2223 mm (1975-76) and 945 mm (1987-88) respectively.

Table 4 The annual characteristics of Jabiru Airport rainfall data

| Statistic | Magnitude | Standard Error |
| :--- | :---: | :---: |
| Mean (mm) | 1,483 | 58.2 |
| Standard deviation (mm) | 302.5 | 41.2 |
| Coefficient of skewness | 0.288 | 0.448 |

Chi-squared test results (test statistic - 0.33/chi-square value ( $0.05 \%$ ) - 7.81) and Kolmogorov Smirnov test results (test statistic $-0.04895 /$ test value -0.256 ) indicate that the annual rainfall data series for Jabiru Airport is normally distributed. The coefficient of skewness of the annual rainfall series is again small. The plot of the observed data and the fitted line are shown in figure 2. The 1:10,000 AEP annual rainfall estimate is 2608 mm with a standard error of 164 mm . The $95 \%$ confidence limit for this estimate, rounded to the nearest 10 mm is $\mathbf{2 6 1 0} \pm \mathbf{3 2 0} \mathbf{~ m m}$. The large standard error and the wider confidence band are due to the short length of the data. The 1975-76 annual rainfall for Jabiru Airport ( 2223 mm ) was tested to determine if it could be treated as an outlier. The test showed 2300 mm as the lower limit for high outliers and hence there is no evidence to exclude the 1975-76 value. However, given the close relationship between the Oenpelli and Jabiru Airport rainfall data (Chiew \& Wang 1999) and the fact that 1975-76 annual rainfall is also the highest annual rainfall for Oenpelli, it is feasible to adopt an AEP of 1 in 88 years (the length of record available at Oenpelli) for the 1975-76 annual rainfall at Jabiru Airport.


Average Recurrence Interval (years)

Figure 2 Distribution of annual rainfall for Jabiru

### 4.3 Summary of analysis of annual rainfall

The best estimate of the $1: 10,000$ AEP annual rainfall for the region considered is $\mathbf{2 4 6 0} \mathbf{~ m m}$ with a standard error of 85 mm using the rainfall data recorded at Oenpelli. It should be noted that the estimate for the $1: 10,000$ AEP annual rainfall using the full Jabiru Airport record $(2610 \mathrm{~mm})$ falls within the confidence limits for the Oenpelli estimate $(2460 \pm 170 \mathrm{~mm})$.

### 4.4 Comparison with estimates made in the Jabiluka EIS

The estimate of the 1:10,000 AEP annual rainfall recommended on page 5-22 of the Jabiluka Project Supplement (Kinhill Engineers 1996) to the draft EIS is 2450 mm . This has been derived from the Jabiru Airport record with the 1975-76 rainfall attributed a recurrence period of 85 years and by hand fitting the probability curve. As indicated above, this is a feasible approach, given the close relationship between the Oenpelli rainfall records and the Jabiru Airport rainfall records. While there is no statistical evidence for treating the 1975/76

Jabiru rainfall as an outlier, the fact that Oenpelli also experienced it's highest annual rainfall report on record in 1975/76 provides some physical justification for reassigning its plotting position. Hand fitting of probability curves is not recommended. It is felt that the analysis of the full record from Oenpelli provides the best estimate of the 1:10,000 AEP annual rainfall. It is interesting to note that the analysis of the Jabiluka Airport annual rainfall data, not including the 1975-76 year, leads to an estimate of the $1: 10,000$ AEP annual rainfall of 2,460 $\pm 290 \mathrm{~mm}$.

## 5 Comment on methodology used

The assumptions involved in the method used were raised at the beginning of the previous section. With respect to the assumption that the distribution of annual rainfalls is normal throughout the entire range of values, it should be noted that uncertainty involved in using this assumption is not accounted for in the $95 \%$ confidence limits stated above.

An alternative method of calculating annual exceedance probability (AEP) from a relatively short record is to calculate expected probability (Institution of Engineers, Australia 1987, Beard 1960). Here, 'expected' is used in the statistical sense and the name would be more precisely expressed as 'Expected Annual Exceedance Probability'. This approach takes the view that one record, such as the Oenpelli record, is just one sample from a normally distributed population, and it can be shown that, on average, over a large number of samples, the expected probability of estimates of the 1 in Y AEP event is always greater than 1 in Y. This implies a higher annual rainfall because it is the rainfall for the expected probability rather than that for the sample probability. The concept is a complex one and the subject is still debated in the literature. However, if the procedures recommended by Beard (1960) are followed, the estimate of the $1: 10,000$ AEP annual rainfall for Oenpelli is 2510 mm . This estimate is not significantly different from the 2460 mm recommended above.

As mentioned earlier in the report, these methods of analysis assume stationarity of the data series being used. In this regard, the proposed analysis of the potential impact of climate change on the $1: 10,000$ AEP annual rainfall by the CSIRO (Jones \& Abbs 1999) will be of interest. If no definitive alteration to the $1: 10,000$ AEP annual rainfall estimate can be made in this regard, one conservative option is to adopt the higher confidence limit of the estimate provided above $(2460+170=2630 \mathrm{~mm})$ as the $1: 10,000$ AEP design annual rainfall.

The above analysis adopted a normal distribution for the annual data series. ERA staff (Kinhill Engineers 1996), in their analysis, have used both a hand fitted probability curve and a log Pearson type III distribution. Hand fitting of probability curves is not recommended because it is subjective and the results are difficult to reproduce. Also, no indication of the accuracy of the estimate can be derived. As shown above, statistical tests applied to the annual series of rainfall data indicate that it can be analysed as a normally distributed data set. It is not clear why ERA have applied a log Pearson type III distribution to annual rainfall from these stations. Applying a logarithmic transformation to the non-skewed initial distribution would have produced a negative skew, but presumably the procedures for dealing with skew, inherent in the (log) Pearson type III approach, handled this effectively and yielded answers much the same as were obtained here.

There is no known method of using annual rainfall data on a regional basis to provide an estimate of the 1 in 10,000 annual rainfall in which we could have greater confidence. It has been suggested that the FORGE (FOcussed Rainfall Growth Estimation) technique, which has been used by Monash University to estimate the 1 in 2,000 short-duration ( 24 hours to 72 hours) rainfalls, may be utilised. However, in this report we are dealing with annual
rainfalls, and as the FORGE methodology has been developed based on rainfall growth or storm growth assumptions it is not applicable in this case. Also, the Hydrological Modelling Study of Water Management at the Jabiluka Site (Chiew \& Wang 1999) has shown the close relationship between the Oenpelli and Jabiru Airport data sets. These facts, and the limited availability of other good-quality long-term rainfall data sets in close proximity to the project site, suggest that the use of a technique similar to FORGE would not provide any additional confidence in the estimate made here.

## 6 Derivation of Probable Maximum Precipitation (PMP) estimates for use in design

### 6.1 6-Minute PMP estimate

### 6.1.1 Derivation of the 6-minute PMP

The 6-minute point-value PMP was estimated using two different techniques:

- Extrapolation of the PMP curve. Point-value PMPs for durations from 15 minutes (the minimum duration normally calculated) to 6 hours were calculated for Jabiluka using the Generalised Short Duration Method (GSDM) (Bureau of Meteorology 1994). Then, each PMP (depth in mm ) was converted to intensity ( $\mathrm{mm} \mathrm{hr}^{-1}$ ) and plotted against duration using linear scales. The best fit to this intensity $v s$. duration curve was a power law $\left(\mathrm{R}^{2}=\right.$ 0.99 ). The curve was extrapolated back to obtain an estimate of the 6 -minute intensity of $1380 \mathrm{~mm} \mathrm{hr}^{-1}$.
- Use of IFD ratio. IFD (Intensity-Frequency-Duration) information was produced for the nearest grid point (Latitude $12.50^{\circ} \mathrm{S}$, Longitude $132.925^{\circ} \mathrm{E}$ ) to Jabiluka. For 100 year ARI, the ratio of the 6 -minute to the 15 -minute intensities (read from the curve) was calculated. The 15 -minute PMP intensity was then multiplied by this ratio to estimate a 6 -minute intensity of $1320 \mathrm{~mm} \mathrm{hr}^{-1}$.

These calculated values differ by less than $4 \%$, lending some confidence to the estimate. In the interest of conservatism, the larger value of $1380 \mathrm{~mm} \mathrm{hr}^{-1}$ is preferred.

### 6.1.2 Recommended 6-minute PMP Estimate

The recommended 6-minute point PMP intensity is $\mathbf{1 , 3 8 0} \mathrm{mm} \mathrm{hr}^{-1}$.
The recommended PMP depth for a 6-minute duration, rounded to the nearest 10 mm , is 140 mm .

### 6.1.3 Comment on the 6-minute PMP Estimate

The 6-minute PMP estimate provided by ERA (on page J3 of Appendix J of the Draft EIS, (Kinhill Engineers 1996)) for the Jabiluka Project is $1150 \mathrm{~mm} \mathrm{hr}^{-1}$. It has not been possible to find out how ERA estimated this value. The 15-minute PMP estimate from the Bureau of Meteorology is $920 \mathrm{~mm} \mathrm{hr}^{-1}$. As expected the intensity of the 6 -minute PMP is greater then that for the 15 -Minute PMP. The difference between the Bureau of Meteorology and ERA estimates ( $+20 \%$ ) is considered significant and the Bureau of Meteorology value of 1380 mm $\mathrm{hr}^{-1}$ should be adopted, particularly as it provides a more conservative approach.

### 6.215 minutes to 72 hours PMP estimates

### 6.2.1 Derivation of $\mathbf{1 5}$ minutes to $\mathbf{7 2}$ hours PMP estimates

Estimates of PMP at the Jabiluka project area can be made for durations of 0.25 to 6 hours using the method as detailed by the Bureau of Meteorology (1994, amended Dec 1996) in Bulletin 53: 'The Estimation of Probable Maximum Precipitation in Australia: Generalised Short Duration Method'. Estimates were made for areas A and B in the project area. Area A represents the $0.09 \mathrm{~km}^{2}$ evaporation pond and, area $B\left(0.17 \mathrm{~km}^{2}\right)$ represents the remainder of the total containment zone for the Jabiluka mill alternative with all tailings being returned to the mine void. The resulting PMP values for areas A and B within the Jabiluka mine site for durations of 0.25 to 6 hours are given in columns 3 of tables 5 and 6 respectively (see figs 3 \& 4 also). The 6 -minute PMP estimate described above is also included in the tables.

Estimates of PMP for durations of 12 to 72 hours at the location of the Jabiluka mine site can be derived from the Generalised Tropical Storm Method (GTSM). The method was developed for those parts of Australia affected by storms of tropical origin (Kennedy (1982) and Kennedy \& Hart (1984)). It is based on storms associated with synoptic weather features, which affect larger areas over longer durations than the storms used in the derivation of the GSDM. The GTSM is applicable to catchments larger than $1 \mathrm{~km}^{2}$ in area. Areas A and B within the Jabiluka project area are both much smaller than $1 \mathrm{~km}^{2}$ in area, having areas of 0.09 and $0.17 \mathrm{~km}^{2}$ respectively. Therefore, it is important to note that the estimates given for durations longer than 6 hours should be used with caution when applied to areas of less than $1 \mathrm{~km}^{2}$.

The resulting GTSM values for a $1 \mathrm{~km}^{2}$ catchment at the location of Areas A and B are shown in columns 4 of tables 5 and 6 . Final PMP values derived from fitting a smooth enveloping curve to this set of estimates are shown in column 5 . Figures 3 and 4 show these enveloping curves for areas A and B respectively.

### 6.2.2 Design temporal distributions of PMP estimates

Figure B. 1 in Appendix B gives the GSDM design temporal distribution appropriate for durations of 0.25 to 6 hours.

Figure B. 2 and table B. 1 in Appendix B give the design temporal distributions of GTSM PMP for durations of 12 to 72 hours.

### 6.2.3 Notional probability of PMP events

The PMP concept, as defined in the introduction, effectively involves zero probability of exceedance. However, estimates made by the various PMP methodologies have a non-zero probability of exceedance. Probabilities of exceedance can therefore be associated with the methodology used to estimate the PMP, not the concept of PMP itself. Kennedy and Hart (1984) used notional AEPs for various PMP methods as a means of indicating the different security levels provided by the different methods. The notional AEPs for the PMP estimation methods are reviewed by Pearce (1994). The AEP for GTSM Remaining Tropical Zone estimates and the revised AEP for GSDM estimates are estimated at approximately $10^{-6}$. With the imminent release of the revised edition of Australian Rainfall and Runoff, Book VI Estimation of Large to Extreme Floods (IE Aust 1998), this advice will be superseded. All future reference to the AEP of the PMP will derive from Book VI.

Table 5 Generalised PMP estimates for area A

| Duration (hours) | Best estimate PMP (mm) | Area A GSDM PMP (mm) | GTSM RTZ 1 SQ KM Area PMP (mm) | Final PMP (mm) |
| :---: | :---: | :---: | :---: | :---: |
| . 1 | 140 | - | - | 140 |
| . 25 | - | 230 | - | 230 |
| . 5 | - | 330 | - | 330 |
| . 75 | - | 430 | - | 430 |
| 1 | - | 530 | - | 530 |
| 1.5 | - | 680 | - | 680 |
| 2 | - | 810 | - | 810 |
| 2.5 | - | 910 | - | 910 |
| 3 | - | 1000 | - | 1000 |
| 4 | - | 1150 | - | 1150 |
| 5 | - | 1250 | - | 1250 |
| 6 | - | 1330 | - | 1330 |
| 12 | - | - | 1050 | 1370 |
| 18 | - | - | - | 1390 |
| 24 | - | - | 1380 | 1460 |
| 36 | - | - | - | 1650 |
| 48 | - | - | 1830 | 1830 |
| 72 | - | - | 2040 | 2040 |

Note: (i) All values are rounded to the nearest 10 mm .
The estimates are for unrestricted durations (ie not 9am to 9am raindays).
The estimates for the 12-, 18-, 24- and 36 -hour durations are interpolated values.

Table 6 Generalised PMP estimates for Area B

| Duration (hours) | Best estimate PMP (mm) | Area B GSDM PMP (mm) | GTSM RTZ 1 SQ KM Area PMP (mm) | Final PMP (mm) |
| :---: | :---: | :---: | :---: | :---: |
| . 1 | 140 | - | - | 140 |
| . 25 | - | 230 | - | 230 |
| . 5 | - | 330 | - | 330 |
| . 75 | - | 420 | - | 420 |
| 1 | - | 520 | - | 520 |
| 1.5 | - | 670 | - | 670 |
| 2 | - | 800 | - | 800 |
| 2.5 | - | 900 | - | 900 |
| 3 | - | 990 | - | 990 |
| 4 | - | 1130 | - | 1130 |
| 5 | - | 1240 | - | 1240 |
| 6 | - | 1320 | - | 1320 |
| 12 | - | - | 1050 | 1370 |
| 18 | - | - | - | 1390 |
| 24 | - | - | 1380 | 1460 |
| 36 | - | - | - | 1650 |
| 48 | - | - | 1830 | 1830 |
| 72 | - | - | 2040 | 2040 |

Note: (i) All values are rounded to the nearest 10 mm .
The estimates are for unrestricted durations (ie not 9am to 9am raindays).
The estimates for the 12-, 18-, 24- and 36 -hour durations are interpolated values.


FIGURE 3 Envelope of Final PMP Depths for Area A within the Jabiluka Mine Site


FIGURE 4 Envelope of Final PMP Depths for Area B within the Jabiluka Mine Site

### 6.2.4 Katherine January 1998 event

It has been suggested that the Katherine 1998 event be examined to determine if further analysis of this event would alter the current estimates of PMP. It should be noted that the Katherine event was not the highest on record in the Katherine Rainfall records. The 48 and 72 hour rainfall totals ( 380.6 mm and 398 mm respectively) were the second highest on record.
However, the 24 hour rainfall total ( 220.8 mm ) was only the $4^{\text {th }}$ highest on record. These rainfalls are considerably less than the PMP estimates for the same durations at Jabiluka and it is unlikely that the analysis of this event would alter the current PMP estimates. It should also be noted that the extreme storms used in the development of the GTSM included storms with significantly greater rainfall then that observed at Katherine in 1998.

## 7 Conclusion

The Bureau of Meteorology has undertaken the above analyses in response to a request from the Supervising Scientist. The results provided are considered by the Bureau to be the best possible given the data limitations and methodologies currently available.

There is close agreement between the Bureau of Meteorology and ERA estimates of the $1: 10,000$ AEP annual rainfall. The Bureau of Meteorology's estimate of the 6-Minute PMP is $20 \%$ greater than that derived by ERA.

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Appendix A

Table A. 1 Monthly and annual rainfall data (mm) for Oenpelli

| Year | Sep | Oct | Nov | Dec | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1910-11 | 35.6 | 49.8 | 60.4 | 371.2 | 348.5 | 287.5 | 73.3 | 341.6 | 0.0 | 0.0 | 0.0 | 0.0 | 1567.9 |
| 1911-12 | 0.0 | 167.7 | 123.6 | 262.2 | 396.8 | 252.6 | 402.2 | 24.4 | 0.0 | 0.0 | 0.0 | 0.0 | 1629.5 |
| 1912-13 | 0.0 | 81.7 | 56.7 | 184.6 | 574.7 | 349.1 | 531.7 | 22.1 | 11.2 | 0.0 | 0.0 | 0.0 | 1811.8 |
| 1913-14 | 0.0 | 0.0 | 55.0 | 178.0 | 388.4 | 164.4 | 459.1 | 31.5 | 42.3 | 0.0 | 0.0 | 0.0 | 1318.7 |
| 1914-15 | 0.0 | 0.0 | 6.4 | 135.9 | 183.4 | 301.3 | 151.8 | 8.6 | 46.0 | 0.0 | 0.0 | 10.2 | 843.6 |
| 1915-16 | 12.2 | 17.5 | 93.2 | 583.3 | 449.3 | 237.5 | 229.6 | 31.7 | 4.1 | 0.0 | 0.0 | 0.0 | 1658.4 |
| 1916-17 | 0.0 | 106.4 | 221.5 | 201.8 | 526.0 | 272.0 | 324.5 | 130.2 | 17.8 | 10.9 | 0.0 | 0.0 | 1811.1 |
| 1917-18 | 11.9 | 114.5 | 127.5 | 248.8 | 336.6 | 505.1 | 115.4 | 33.9 | 19.8 | 0.0 | 0.0 | 0.0 | 1513.5 |
| 1918-19 | 0.0 | 6.4 | 61.4 | 144.3 | 776.7 | 215.7 | 358.5 | 111.6 | 0.0 | 0.0 | 0.0 | 0.0 | 1674.6 |
| 1919-20 | 3.8 | 0.0 | 56.3 | 165.6 | 223.6 | 488.5 | 75.2 | 94.0 | 0.0 | 2.3 | 0.0 | 0.0 | 1109.3 |
| 1920-21 | 0.0 | 3.8 | 88.8 | 262.8 | 389.3 | 239.6 | 384.1 | 37.1 | 0.0 | 0.0 | 2.3 | 0.0 | 1407.8 |
| 1921-22 | 0.0 | 63.5 | 157.4 | 314.9 | 406.7 | 336.9 | 314.0 | 28.5 | 0.0 | 0.0 | 3.0 | 0.0 | 1624.9 |
| 1922-23 | 0.0 | 77.2 | 86.8 | 166.4 | 288.9 | 178.4 | 533.1 | 96.7 | 16.4 | 0.0 | 0.0 | 0.0 | 1443.9 |
| 1923-24 | 0.0 | 13.9 | 60.9 | 528.8 | 175.1 | 176.4 | 230.1 | 2.8 | 2.8 | 0.0 | 1.0 | 0.0 | 1191.8 |
| 1924-25 | 0.0 | 5.9 | 157.0 | 244.2 | 269.3 | 280.2 | 303.1 | 208.4 | 1.1 | 0.0 | 0.0 | 0.0 | 1469.2 |
| 1925-26 | 0.0 | 1.8 | 10.9 | 55.2 | 372.4 | 210.2 | 156.4 | 10.6 | 0.5 | 0.0 | 0.0 | 0.0 | 818.0 |
| 1926-27 | 0.3 | 45.5 | 110.0 | 258.3 | 234.5 | 271.1 | 223.8 | 56.9 | 4.6 | 1.3 | 0.0 | 0.0 | 1206.3 |
| 1927-28 | 2.3 | 101.5 | 222.4 | 323.0 | 134.8 | 196.3 | 351.3 | 26.9 | 0.0 | 0.0 | 0.0 | 0.0 | 1358.5 |
| 1928-29 | 0.0 | 0.0 | 98.3 | 142.9 | 245.3 | 295.0 | 287.4 | 98.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1166.9 |
| 1929-30 | 0.0 | 0.0 | 193.8 | 161.9 | 310.3 | 499.7 | 593.6 | 11.7 | 0.0 | 0.0 | 0.0 | 0.0 | 1771.0 |
| 1930-31 | 0.0 | 0.0 | 91.5 | 242.4 | 352.0 | 218.9 | 291.5 | 48.5 | 0.8 | 0.0 | 0.0 | 0.0 | 1245.6 |
| 1931-32 | 0.0 | 0.0 | 190.8 | 193.0 | 460.7 | 176.9 | 514.5 | 30.0 | 5.6 | 0.0 | 0.0 | 0.0 | 1571.5 |
| 1932-33 | 0.0 | 9.6 | 128.0 | 179.2 | 290.5 | 234.2 | 298.5 | 4.6 | 0.0 | 34.7 | 0.0 | 0.0 | 1179.3 |


| Year | Sep | Oct | Nov | Dec | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1933-34 | 2.5 | 30.0 | 91.6 | 299.7 | 281.3 | 264.1 | 473.1 | 49.0 | 24.3 | 0.0 | 0.0 | 0.0 | 1515.6 |
| 1934-35 | 22.1 | 22.6 | 56.3 | 183.6 | 333.0 | 150.9 | 301.8 | 4.3 | 0.3 | 20.0 | 0.0 | 0.0 | 1094.9 |
| 1935-36 | 0.0 | 2.0 | 71.4 | 189.1 | 242.5 | 280.1 | 225.5 | 11.4 | 0.0 | 0.0 | 41.9 | 0.0 | 1063.9 |
| 1936-37 | 0.0 | 21.6 | 59.4 | 269.8 | 272.1 | 242.5 | 306.8 | 31.5 | 0.0 | 0.0 | 0.0 | 0.0 | 1203.7 |
| 1937-38 | 3.3 | 19.1 | 86.7 | 129.9 | 378.0 | 497.8 | 101.3 | 68.3 | 10.6 | 1.5 | 0.0 | 0.0 | 1296.5 |
| 1938-39 | 0.0 | 10.9 | 169.6 | 134.5 | 391.3 | 186.2 | 245.9 | 24.7 | 1.0 | 5.1 | 0.0 | 0.0 | 1169.2 |
| 1939-40 | 0.0 | 6.7 | 74.9 | 122.3 | 520.9 | 221.3 | 418.4 | 64.5 | 8.6 | 0.0 | 0.0 | 0.0 | 1437.6 |
| 1940-41 | 0.0 | 0.0 | 58.4 | 231.4 | 397.1 | 273.6 | 240.8 | 101.4 | 10.7 | 0.5 | 0.0 | 0.0 | 1313.9 |
| 1941-42 | 0.3 | 1.0 | 97.5 | 92.8 | 232.7 | 248.2 | 47.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 720.3 |
| 1942-43 | 9.7 | 69.4 | 76.3 | 374.9 | 228.1 | 639.7 | 112.2 | 93.4 | 0.0 | 0.0 | 0.0 | 0.0 | 1603.7 |
| 1943-44 | 0.0 | 4.1 | 276.5 | 214.1 | 214.1 | 281.8 | 243.6 | 48.2 | 0.0 | 0.0 | 0.0 | 0.0 | 1282.4 |
| 1944-45 | 0.0 | 0.0 | 114.6 | 352.1 | 334.3 | 234.8 | 312.5 | 69.0 | 23.9 | 0.0 | 0.0 | 0.0 | 1441.2 |
| 1945-46 | 10.9 | 19.1 | 40.8 | 206.1 | 245.9 | 384.5 | 211.1 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 1118.7 |
| 1946-47 | 0.3 | 0.5 | 53.6 | 118.6 | 190.1 | 362.4 | 284.6 | 44.8 | 3.3 | 0.5 | 0.0 | 1.6 | 1060.3 |
| 1947-48 | 32.8 | 26.7 | 91.8 | 179.2 | 153.1 | 279.6 | 98.0 | 413.9 | 2.3 | 0.0 | 0.0 | 0.0 | 1277.4 |
| 1948-49 | 0.0 | 0.0 | 276.4 | 196.1 | 258.1 | 214.1 | 353.2 | 44.7 | 0.0 | 0.0 | 0.0 | 0.0 | 1342.6 |
| 1949-50 | 0.0 | 9.0 | 178.5 | 237.6 | 447.3 | 320.0 | 164.8 | 34.2 | 0.3 | 0.0 | 0.0 | 0.0 | 1391.7 |
| 1950-51 | 18.1 | 81.9 | 199.5 | 395.4 | 197.3 | 231.2 | 135.1 | 3.6 | 0.0 | 0.0 | 0.0 | 0.3 | 1262.4 |
| 1951-52 | 0.3 | 59.7 | 19.1 | 129.3 | 257.4 | 113.4 | 174.9 | 0.0 | 18.8 | 0.0 | 0.0 | 0.0 | 772.9 |
| 1952-53 | 0.0 | 19.8 | 163.3 | 142.2 | 285.2 | 167.7 | 194.6 | 169.7 | 0.0 | 0.0 | 0.0 | 0.0 | 1142.5 |
| 1953-54 | 0.0 | 17.8 | 86.0 | 176.9 | 332.1 | 192.9 | 274.4 | 257.5 | 0.0 | 0.0 | 0.0 | 0.0 | 1337.6 |
| 1954-55 | 0.0 | 102.5 | 30.2 | 152.4 | 227.9 | 347.3 | 165.3 | 72.3 | 66.5 | 7.2 | 21.1 | 0.0 | 1192.7 |
| 1955-56 | 0.0 | 34.5 | 232.2 | 65.7 | 310.4 | 420.2 | 341.4 | 143.1 | 89.8 | 0.3 | 63.2 | 5.8 | 1706.6 |
| 1956-57 | 0.5 | 51.6 | 158.0 | 248.2 | 399.2 | 353.9 | 491.2 | 72.4 | 1.8 | 0.0 | 0.0 | 0.0 | 1776.8 |


| Year | Sep | Oct | Nov | Dec | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1957-58 | 0.0 | 0.8 | 68.8 | 319.5 | 246.7 | 225.7 | 278.7 | 86.9 | 99.2 | 8.7 | 1.3 | 3.8 | 1340.1 |
| 1958-59 | 0.0 | 19.9 | 148.3 | 120.3 | 323.0 | 279.5 | 216.8 | 339.8 | 21.2 | 0.0 | 0.0 | 0.0 | 1468.8 |
| 1959-60 | 0.0 | 0.0 | 31.5 | 272.1 | 317.1 | 296.6 | 336.8 | 43.3 | 21.9 | 0.0 | 0.3 | 0.3 | 1319.9 |
| 1960-61 | 14.7 | 2.8 | 95.6 | 244.8 | 373.6 | 155.7 | 74.3 | 10.0 | 0.0 | 0.0 | 19.8 | 0.0 | 991.3 |
| 1961-62 | 0.0 | 20.4 | 75.6 | 163.9 | 497.4 | 654.9 | 57.3 | 12.7 | 0.0 | 0.6 | 0.0 | 0.0 | 1482.8 |
| 1962-63 | 12.8 | 53.6 | 54.2 | 281.6 | 213.0 | 263.3 | 207.4 | 86.7 | 1.0 | 0.0 | 0.0 | 0.0 | 1173.6 |
| 1963-64 | 0.0 | 0.0 | 56.4 | 276.2 | 416.1 | 379.7 | 415.1 | 142.1 | 11.7 | 0.3 | 0.0 | 0.0 | 1697.6 |
| 1964-65 | 16.5 | 93.1 | 248.5 | 166.7 | 365.1 | 350.7 | 529.8 | 0.3 | 6.4 | 0.6 | 0.0 | 0.0 | 1777.7 |
| 1965-66 | 0.0 | 1.0 | 3.0 | 502.8 | 276.3 | 236.4 | 169.2 | 3.2 | 0.0 | 0.0 | 0.0 | 0.0 | 1191.9 |
| 1966-67 | 0.0 | 26.4 | 100.5 | 195.6 | 217.9 | 480.6 | 158.4 | 34.8 | 0.6 | 0.3 | 0.0 | 0.0 | 1215.1 |
| 1967-68 | 0.0 | 0.5 | 39.5 | 164.6 | 401.2 | 507.3 | 161.5 | 69.1 | 193.6 | 0.0 | 2.0 | 14.2 | 1553.5 |
| 1968-69 | 0.0 | 1.8 | 59.2 | 267.1 | 426.5 | 633.3 | 490.5 | 0.0 | 1.0 | 0.0 | 0.0 | 0.0 | 1879.4 |
| 1969-70 | 0.5 | 15.0 | 120.3 | 241.3 | 277.7 | 196.1 | 154.7 | 13.4 | 1.3 | 0.0 | 0.0 | 0.0 | 1020.3 |
| 1970-71 | 26.2 | 10.4 | 148.4 | 138.8 | 287.2 | 251.2 | 442.7 | 92.2 | 2.5 | 0.0 | 0.0 | 0.0 | 1399.6 |
| 1971-72 | 16.8 | 91.2 | 125.9 | 362.5 | 246.2 | 407.1 | 312.3 | 26.7 | 12.5 | 0.0 | 0.0 | 0.0 | 1601.2 |
| 1972-73 | 0.0 | 0.0 | 151.5 | 106.1 | 531.7 | 216.5 | 183.1 | 29.7 | 8.1 | 41.2 | 0.0 | 0.0 | 1267.9 |
| 1973-74 | 1.8 | 2.8 | 366.1 | 231.9 | 465.8 | 255.8 | 301.0 | 84.6 | 39.6 | 0.0 | 0.0 | 10.6 | 1760.0 |
| 1974-75 | 0.2 | 15.4 | 100.8 | 359.2 | 188.7 | 526.3 | 441.0 | 153.7 | 0.0 | 0.0 | 0.0 | 0.0 | 1785.3 |
| 1975-76 | 10.2 | 80.2 | 132.6 | 298.4 | 320.0 | 491.3 | 545.9 | 130.4 | 2.6 | 0.0 | 0.0 | 0.0 | 2011.6 |
| 1976-77 | 1.2 | 84.9 | 125.4 | 188.8 | 480.6 | 329.8 | 454.8 | 75.6 | 12.5 | 0.0 | 0.0 | 0.0 | 1753.6 |
| 1977-78 | 0.0 | 0.0 | 71.8 | 190.0 | 220.9 | 414.6 | 131.1 | 76.4 | 49.2 | 3.2 | 12.8 | 0.0 | 1170.0 |
| 1978-79 | 7.0 | 70.4 | 142.7 | 217.6 | 399.8 | 320.4 | 248.2 | 27.2 | 0.0 | 0.0 | 0.2 | 0.0 | 1433.5 |
| 1979-80 | 0.0 | 39.4 | 44.4 | 160.6 | 546.4 | 530.8 | 320.8 | 50.2 | 10.8 | 0.0 | 0.0 | 5.0 | 1708.4 |
| 1980-81 | 0.0 | 17.4 | 31.5 | 167.8 | 360.4 | 547.8 | 601.8 | 28.4 | 16.0 | 0.0 | 4.8 | 0.1 | 1776.0 |


| Year | Sep | Oct | Nov | Dec | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1981-82 | 26.8 | 22.5 | 309.3 | 286.0 | 337.9 | 384.9 | 218.2 | 15.0 | 1.0 | 0.0 | 0.0 | 0.0 | 1601.6 |
| 1982-83 | 4.4 | 0.0 | 42.8 | 85.8 | 173.6 | 209.4 | 528.7 | 166.1 | 54.8 | 0.0 | 0.0 | 0.0 | 1265.6 |
| 1983-84 | 0.0 | 27.6 | 96.4 | 68.8 | 261.8 | 626.8 | 464.4 | 2.4 | 6.2 | 0.0 | 0.0 | 0.0 | 1554.4 |
| 1984-85 | 70.2 | 13.0 | 82.4 | 432.2 | 267.4 | 292.2 | 332.6 | 390.2 | 0.0 | 0.4 | 0.0 | 0.0 | 1880.6 |
| 1985-86 | 7.2 | 0.8 | 135.6 | 185.2 | 524.6 | 191.4 | 118.6 | 85.8 | 0.0 | 0.0 | 40.8 | 19.2 | 1309.2 |
| 1986-87 | 14.2 | 65.2 | 101.4 | 142.8 | 342.8 | 383.3 | 169.2 | 37.8 | 1.2 | 0.0 | 0.0 | 0.0 | 1257.9 |
| 1987-88 | 0.0 | 1.2 | 79.0 | 206.4 | 208.2 | 201.2 | 298.4 | 69.4 | 57.2 | 0.0 | 0.0 | 0.0 | 1121.0 |
| 1988-89 | 0.0 | 0.4 | 184.2 | 233.2 | 156.0 | 232.0 | 409.2 | 210.0 | 62.8 | 0.0 | 0.2 | 0.0 | 1488.0 |
| 1989-90 | 0.0 | 3.8 | 88.0 | 157.0 | 266.3 | 153.8 | 256.0 | 99.0 | 91.0 | 2.2 | 0.0 | 0.0 | 1117.1 |
| 1990-91 | 0.0 | 0.0 | 40.2 | 193.8 | 700.4 | 657.8 | 132.4 | 71.8 | 0.0 | 0.0 | 0.0 | 0.0 | 1796.4 |
| 1991-92 | 0.0 | 0.0 | 50.8 | 65.9 | 243.3 | 385.7 | 134.4 | 64.8 | 0.0 | 0.0 | 0.0 | 0.0 | 944.9 |
| 1992-93 | 42.8 | 8.4 | 54.6 | 245.3 | 350.2 | 587.0 | 179.0 | 11.0 | 1.7 | 0.0 | 0.0 | 0.0 | 1480.0 |
| 1993-94 | 2.2 | 5.0 | 110.7 | 164.5 | 203.8 | 255.2 | 239.0 | 105.4 | 4.1 | 0.0 | 0.0 | 0.0 | 1089.9 |
| 1994-95 | 0.0 | 13.0 | 12.5 | 304.6 | 750.1 | 478.0 | 275.0 | 162.2 | 3.3 | 0.6 | 0.0 | 0.0 | 1999.3 |
| 1995-96 | 0.0 | 34.1 | 61.9 | 257.0 | 213.6 | 243.8 | 186.8 | 240.5 | 5.4 | 0.0 | 0.0 | 0.0 | 1243.1 |
| 1996-97 | 0.0 | 5.7 | 87.8 | 329.5 | 549.6 | 317.0 | 234.7 | 2.9 | 5.1 | 0.0 | 0.0 | 0.0 | 1532.3 |
| 1997-98 | 0.0 | 14.4 | 104.9 | 258.7 | 522.1 | 328.9 | 121.1 | 191.6 | 13.3 | 0.0 | 0.0 | 1.5 | 1556.5 |
| 1998-99 | 8.0 | 60.3 | 156.0 | 334.7 | 245.5 |  |  |  |  |  |  |  |  |
| Monthly Average | 5.2 | 26.4 | 107.9 | 225.9 | 337.4 | 321.8 | 277.2 | 77.7 | 14.2 | 1.6 | 2.5 | 0.8 | 1399.5 |
| Highest | 70.2 | 167.7 | 366.1 | 583.3 | 776.7 | 657.8 | 601.8 | 413.9 | 193.6 | 41.2 | 63.2 | 19.2 | 2011.6 |
| Lowest | 0.0 | 0.0 | 3.0 | 55.2 | 134.8 | 113.4 | 47.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 720.3 |
| Number of Years | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 88 | 88 | 88 | 88 | 88 |

Table A. 2 Monthly and annual rainfall data (mm) for Jabiru Airport

| Water Year | SEP | OCT | NOV | DEC | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | Total | Water Year |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1971/72 | 1 | 51 | 108 | 168 | 192 | 237 | 344 | 11 | 18 | 0 | 0 | 0 | 1129 | 1971/72 |
| 1972/73 | 0 | 2 | 188 | 157 | 460 | 117 | 464 | 49 | 7 | 39 | 0 | 0 | 1482 | 1972/73 |
| 1973/74 | 0 | 44 | 332 | 167 | 468 | 275 | 348 | 73 | 25 | 0 | 0 | 22 | 1754 | 1973/74 |
| 1974/75 | 0 | 17 | 174 | 218 | 270 | 431 | 250 | 178 | 0 | 0 | 0 | 0 | 1538 | 1974/75 |
| 1975/76 | 1 | 206 | 113 | 381 | 394 | 503 | 590 | 34 | 0 | 0 | 0 | 0 | 2223 | 1975/76 |
| 1976/77 | 0 | 52 | 182 | 142 | 342 | 193 | 376 | 95 | 13 | 0 | 0 | 0 | 1395 | 1976/77 |
| 1977/78 | 0 | 6 | 97 | 408 | 329 | 425 | 147 | 23 | 10 | 0 | 5 | 0 | 1448 | 1977/78 |
| 1978/79 | 27 | 20 | 204 | 302 | 470 | 322 | 154 | 4 | 3 | 0 | 0 | 0 | 1504 | 1978/79 |
| 1979/80 | 0 | 26 | 118 | 139 | 506 | 768 | 268 | 64 | 5 | 0 | 0 | 0 | 1895 | 1979/80 |
| 1980/81 | 0 | 25 | 49 | 348 | 325 | 386 | 457 | 18 | 16 | 0 | 0 | 3 | 1627 | 1980/81 |
| 1981/82 | 26 | 41 | 277 | 259 | 364 | 228 | 288 | 2 | 0 | 0 | 0 | 0 | 1485 | 1981/82 |
| 1982/83 | 0 | 0 | 69 | 148 | 188 | 131 | 469 | 175 | 14 | 0 | 0 | 0 | 1195 | 1982/83 |
| 1983/84 | 2 | 49 | 159 | 72 | 308 | 645 | 409 | 13 | 8 | 0 | 5 | 0 | 1671 | 1983/84 |
| 1984/85 | 81 | 4 | 224 | 348 | 311 | 278 | 286 | 217 | 0 | 9 | 0 | 0 | 1758 | 1984/85 |
| 1985/86 | 4 | 0 | 169 | 191 | 396 | 104 | 205 | 108 | 1 | 0 | 37 | 7 | 1222 | 1985/86 |
| 1986/87 | 16 | 51 | 92 | 139 | 339 | 551 | 89 | 30 | 9 | 0 | 0 | 0 | 1315 | 1986/87 |
| 1987/88 | 0 | 2 | 116 | 133 | 226 | 179 | 271 | 15 | 1 | 0 | 0 | 0 | 945 | 1987/88 |
| 1988/89 | 0 | 28 | 216 | 258 | 245 | 216 | 391 | 60 | 1 | 0 | 0 | 0 | 1415 | 1988/89 |
| 1989/90 | 0 | 33 | 88 | 157 | 251 | 157 | 202 | 51 | 90 | 0 | 0 | 0 | 1029 | 1989/90 |
| 1990/91 | 0 | 0 | 78 | 203 | 458 | 396 | 85 | 149 | 0 | 0 | 0 | 0 | 1370 | 1990/91 |
| 1991/92 | 0 | 0 | 199 | 85 | 210 | 345 | 128 | 48 | 1 | 0 | 0 | 0 | 1017 | 1991/92 |
| 1992/93 | 20 | 97 | 40 | 156 | 461 | 290 | 125 | 36 | 1 | 0 | 0 | 0 | 1225 | 1992/93 |


| 1993/94 | 3 | 2 | 50 | 467 | 324 | 455 | 198 | 105 | 1 | 0 | 0 | 0 | 1606 | 1993/94 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1994/95 | 0 | 10 | 87 | 344 | 749 | 258 | 171 | 117 | 11 | 8 | 0 | 0 | 1754 | 1994/95 |
| 1995/96 | 0 | 9 | 90 | 342 | 329 | 270 | 189 | 192 | 8 | 0 | 0 | 0 | 1429 | 1995/96 |
| 1996/97 | 0 | 27 | 128 | 392 | 807 | 387 | 208 | 0 | 0 | 0 | 0 | 0 | 1950 | 1996/97 |
| 1997/98 | 0 | 4 | 182 | 313 | 520 | 311 | 151 | 186 | 0 | 0 | 0 | 0 | 1667 | 1997/98 |
| 1998/99 | 2 | 210 | 196 | 332 | 314 |  |  |  |  |  |  |  |  | 1998/99 |
| Maximum | 81 | 206 | 332 | 467 | 807 | 768 | 590 | 217 | 90 | 39 | 37 | 22 | 2223 | Maximum |
| Minimum | 0 | 0 | 40 | 72 | 188 | 104 | 85 | 0 | 0 | 0 | 0 | 0 | 945 | Minimum |
| Mean | 7 | 30 | 142 | 238 | 379 | 328 | 269 | 76 | 9 | 2 | 2 | 1 | 1483 | Mean |

## Appendix B



Figure B. 1 GSDM design temporal distribution for 0.25 to 6 hours.


Figure B. 2 GTSM PMP (RTZ) design temporal distributions for durations of 12 to 72 hours

Table B. 1 GTSM remaining tropical zone design temporal distributions
Table B.1(i) Temporal distribution for a 12-hour duration

| Time \% | Cumulative \% |
| :---: | :---: |
| 2.5 | 0.4 |
| 5.0 | 1.0 |
| 7.5 | 1.8 |
| 10.0 | 2.7 |
| 12.5 | 3.9 |
| 15.0 | 5.3 |
| 17.5 | 7.3 |
| 20.0 | 9.5 |
| 22.5 | 12.0 |
| 25.0 | 14.5 |
| 27.5 | 17.4 |
| 30.0 | 20.3 |
| 32.5 | 23.5 |
| 35.0 | 27.0 |
| 37.5 | 30.5 |
| 40.0 | 33.9 |
| 42.5 | 37.7 |
| 45.0 | 41.4 |
| 47.5 | 45.2 |
| 50.0 | 49.0 |
| 52.5 | 52.7 |
| 55.0 | 56.5 |
| 57.5 | 60.2 |
| 60.0 | 63.6 |
| 62.5 | 66.8 |
| 65.0 | 70.1 |
| 67.5 | 73.3 |
| 70.0 | 76.4 |
| 72.5 | 79.4 |
| 75.0 | 82.4 |
| 77.5 | 85.1 |
| 80.0 | 87.6 |
| 82.5 | 90.2 |
| 85.0 | 92.5 |
| 87.5 | 94.4 |
| 90.0 | 96.1 |
| 92.5 | 97.5 |
| 95.0 | 98.5 |
| 100.0 | 100.0 |

Table B.1(ii) Temporal distribution for a 24-hour duration

| Time \% | Cumulative \% |
| :---: | :---: |
| 5.0 | 1.6 |
| 7.5 | 2.7 |
| 10.0 | 4.1 |
| 12.5 | 5.7 |
| 15.0 | 7.6 |
| 17.5 | 10.0 |
| 20.0 | 12.3 |
| 22.5 | 15.2 |
| 25.0 | 18.2 |
| 27.5 | 21.4 |
| 30.0 | 24.7 |
| 32.5 | 28.1 |
| 35.0 | 31.6 |
| 37.5 | 35.3 |
| 40.0 | 39.1 |
| 42.5 | 43.2 |
| 45.0 | 47.2 |
| 47.5 | 51.3 |
| 50.0 | 55.2 |
| 52.5 | 58.9 |
| 55.0 | 62.6 |
| 57.5 | 66.1 |
| 60.0 | 69.5 |
| 62.5 | 72.9 |
| 65.0 | 75.9 |
| 67.5 | 78.8 |
| 70.0 | 81.5 |
| 72.5 | 84.0 |
| 75.0 | 86.4 |
| 77.5 | 88.4 |
| 80.0 | 90.5 |
| 82.5 | 92.3 |
| 85.0 | 93.8 |
| 87.5 | 95.3 |
| 90.0 | 96.6 |
| 92.5 | 97.8 |
| 95.0 | 98.6 |
| 100.0 | 100.0 |

Table B.1(iii) Temporal distribution for a 36-hour duration

| Time \% | Cumulative \% |
| :---: | :---: |
| 5.0 | 1.9 |
| 7.5 | 3.4 |
| 10.0 | 5.2 |
| 12.5 | 7.4 |
| 15.0 | 10.0 |
| 17.5 | 13.0 |
| 20.0 | 16.1 |
| 22.5 | 19.5 |
| 25.0 | 23.2 |
| 27.5 | 27.0 |
| 30.0 | 30.6 |
| 32.5 | 34.6 |
| 35.0 | 38.6 |
| 37.5 | 42.8 |
| 40.0 | 46.9 |
| 42.5 | 50.8 |
| 45.0 | 54.5 |
| 47.5 | 58.5 |
| 50.0 | 62.4 |
| 52.5 | 65.9 |
| 55.0 | 69.6 |
| 57.5 | 73.0 |
| 60.0 | 76.3 |
| 62.5 | 79.3 |
| 65.0 | 81.9 |
| 67.5 | 84.3 |
| 70.0 | 86.4 |
| 72.5 | 88.3 |
| 75.0 | 90.0 |
| 77.5 | 91.5 |
| 80.0 | 92.9 |
| 82.5 | 94.2 |
| 85.0 | 95.4 |
| 87.5 | 96.5 |
| 90.0 | 97.4 |
| 92.5 | 98.3 |
| 95.0 | 99.0 |
| 100.0 | 100.0 |

Table B.1(iv) Temporal distribution for a 48-hour duration

| Time \% | Cumulative \% |
| :---: | :---: |
| 2.5 | 1.2 |
| 5.0 | 2.9 |
| 7.5 | 5.2 |
| 10.0 | 7.8 |
| 12.5 | 10.8 |
| 15.0 | 14.2 |
| 17.5 | 17.9 |
| 20.0 | 21.9 |
| 22.5 | 26.2 |
| 25.0 | 30.9 |
| 27.5 | 36.0 |
| 30.0 | 40.5 |
| 32.5 | 45.0 |
| 35.0 | 49.4 |
| 37.5 | 53.6 |
| 40.0 | 57.6 |
| 42.5 | 61.4 |
| 45.0 | 65.0 |
| 47.5 | 68.2 |
| 50.0 | 71.4 |
| 52.5 | 74.3 |
| 55.0 | 77.0 |
| 57.5 | 79.5 |
| 60.0 | 81.8 |
| 62.5 | 83.8 |
| 65.0 | 85.7 |
| 7.5 | 87.4 |
| 70.0 | 88.7 |
| 72.5 | 90.2 |
| 75.0 | 91.5 |
| 77.5 | 92.7 |
| 80.0 | 93.8 |
| 82.5 | 94.9 |
| 85.0 | 95.9 |
| 87.5 | 96.9 |
| 90.0 | 97.8 |
| 92.5 | 98.7 |
| 95.0 | 99.3 |
| 100.0 | 100.0 |

Table B.1(v) Temporal distribution for a 72-hour duration

| Time \% | Cumulative \% |
| :---: | :---: |
| 2.5 | 2.1 |
| 5.0 | 4.7 |
| 7.5 | 7.8 |
| 10.0 | 11.7 |
| 12.5 | 16.1 |
| 15.0 | 21.3 |
| 17.5 | 26.5 |
| 20.0 | 32.5 |
| 22.5 | 38.5 |
| 25.0 | 44.3 |
| 27.5 | 49.9 |
| 30.0 | 55.0 |
| 32.5 | 60.2 |
| 35.0 | 64.0 |
| 37.5 | 67.2 |
| 40.0 | 69.9 |
| 42.5 | 72.4 |
| 45.0 | 74.7 |
| 47.5 | 76.7 |
| 50.0 | 78.5 |
| 52.5 | 80.4 |
| 55.0 | 82.1 |
| 57.5 | 83.7 |
| 60.0 | 85.1 |
| 62.5 | 86.5 |
| 65.0 | 87.8 |
| 67.5 | 89.1 |
| 70.0 | 90.3 |
| 72.5 | 91.5 |
| 75.0 | 92.7 |
| 77.5 | 93.6 |
| 80.0 | 94.7 |
| 82.5 | 95.7 |
| 85.0 | 96.6 |
| 87.5 | 97.5 |
| 90.0 | 98.2 |
| 92.5 | 98.8 |
| 95.0 | 99.4 |
| 100.0 | 100.0 |

